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# The optimization of methanol yield in direct selective oxidation of methane with $O_2$ and NO in the presence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub>

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### Abstract

Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst was examined for the enhancement of methanol selectivity in the products of the direct selective oxidation of methane with O<sub>2</sub> and NO in the gas-phase. The precise study of effects of reaction pressures and CH<sub>4</sub>/O<sub>2</sub> ratio on the yield of CH<sub>3</sub>OH was performed with the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. The yield of CH<sub>3</sub>OH had a maximum value at 0.4 MPa and CH<sub>4</sub>/O<sub>2</sub> = 8.0. The yield of CH<sub>3</sub>OH was enhanced with the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst in all of the examined regions. © 2002 Elsevier Science B.V. All rights reserved.

Keywords: Selective oxidation; Methane; Cu-ZnO catalyst; Methanol; Hydrogenation

### 1. Introduction

Direct oxidation of methane to  $C_1$ -oxygenates (methanol and formaldehyde) with oxygen is a potentially important process not only for the effective use of natural gas resources, but also for minimization of energy consumption. Various researches of non-catalytic or catalytic oxidation of methane to oxygenates have been carried out since early last century, but the main products were still carbon oxides [1–4]. The rate-determining step of the direct selective oxidation of methane is the first hydrogen abstraction from

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methane. Therefore, many researches using initiators or sensitizers have been carried out in order to reduce the activation energy of the first hydrogen abstraction from methane. NO<sub>x</sub> (x = 1, 2) has been reported as an effective initiator for the activation of methane [5-9]. Recently, Teng et al. [10] and Tabata et al. [11] systematically examined the effects of variation of reaction conditions on the yield of C<sub>1</sub>-oxygenates in gas-phase selective oxidation of methane with O<sub>2</sub> and NO<sub>x</sub> (x = 1, 2). The selectivity of both methanol and formaldehyde depended strongly on their reaction conditions, i.e.  $NO_x$  concentration,  $CH_4/O_2$  ratio in the feed gas and space velocity (SV), these two C<sub>1</sub>-oxygenates were always observed more or less in all the examined regions. It is quite worthwhile to control the selectivities of methanol and formaldehyde in the products for the application to a practical process for the gas-phase selective oxidation of methane.

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Very recently, we tried to enhance the selectivity of methanol in the products using a Cu-ZnO based catalyst in addition to the gas-phase selective oxidation of methane with O<sub>2</sub> and NO [12-14]. Both CH<sub>3</sub>OH and CH<sub>2</sub>O were observed as C<sub>1</sub>-oxygenates at 550 °C in the gas-phase selective oxidation of methane with O<sub>2</sub> and NO, but only CH<sub>3</sub>OH was observed in the products as C1-oxygenate in the presence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst at 250 °C in addition to the gas-phase reaction at 550 °C. We suggested that the formation of CH<sub>3</sub>OH through the hydrogenation of CH<sub>2</sub>O and the water gas shift reaction (WGSR) of CO-H<sub>2</sub>O progressed simultaneously on the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst [12]. Furthermore, we suggested that the complete exhaustion of oxygen in the region of gas-phase reaction was a key for the effective use of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. All the reactions were carried out at 0.5 MPa so as to use up oxygen during the gas-phase reaction. The highest yield of CH<sub>3</sub>OH was around 1.6% at 0.5 MPa in the presence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst, and this value was smaller than that of total oxygenates (ca. 6%) at 0.1 MPa in the absence of the catalyst [10]. The higher ratio of  $CH_4/O_2$  in the feed gas ( $CH_4/O_2 = 13.3$ ) at 0.5 MPa in comparison to the ratio at 0.1 MPa  $(CH_4/O_2 = 2.0)$  was assumed to retard the yield of  $CH_3OH$  in the products. This higher value of  $CH_4/O_2$ was selected so as to avoid explosions.

We consider that the precise study of variation effects of reaction pressures and  $CH_4/O_2$  ratio on the yield of  $CH_3OH$  is worthwhile for enhancing the  $CH_3OH$  selectivity. We therefore examine the catalytic performance of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst under various reaction pressures and  $CH_4/O_2$  ratios so as to optimize methanol yield.

## 2. Experimental

### 2.1. CH<sub>4</sub>–O<sub>2</sub>–NO reaction

Highly purified methane (>99.9995%), oxygen (>99.9999%), and 3.0% NO (Ar balance) were mixed with argon (>99.9999%). The standard feed gas composition (CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, 16.2%) was controlled with a mass flow controller. A quartz tube (7 mm i.d.) was mounted inside of a stainless tube (13.8 mm o.d.) in order to minimize the

effects of reactor wall. This quartz tube was heated for the gas-phase selective oxidation of methane with an electric furnace from the outside of the stainless tube, the length of the heated zone was 100 mm. The temperature of gas-phase reaction was measured at the center part of the electric furnace with a thermocouple, which was mounted at the center part of the reactor. The thermocouple was covered with a quartz tube (3 mm o.d.) so as to avoid any reactions on the surface of the thermocouple. The same Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst in the previous work [12] was used. The catalyst was mounted at 150 mm downstream from the end of the heater. The temperature of catalyst was measured from the outside of the reactor with a thermocouple. The temperature of the mounted catalyst was less than 150°C during the gas-phase reaction at 550 °C. We prepared the second heater and controlled the temperature of the catalyst at 250 °C. The length of this heater was 100 mm.

We used mechanical seals for connecting the quartz tube and the stainless one, avoiding direct contact between reaction gas and the stainless tube. Flow rate of feed gas was stabilized at  $120 \text{ ml min}^{-1}$  (SV =  $15700 \,\mathrm{h^{-1}}$ ). The SV was calculated by dividing the gas flow volume per 1 h at 25 °C and atmospheric pressure by the volume of the catalyst (0.5 g). The mixed gas was fed from the bottom side of the reactor. Products were analyzed with two on-line gas chromatography. CO, CO<sub>2</sub>, ethane, ethene, CH<sub>2</sub>O, CH<sub>3</sub>OH and nitromethane were detected with FID (Gaskuropack 54) using a methanator. Methane, hydrogen and oxygen were detected with TCD (activated carbon). Carbon balance between the reactants and the products exceeded 95%. Every feed gas was mixed just before the inlet of the reactor. All of the gas lines from the exit of the reactor up to the gas chromatograph were heated at 120 °C in order to avoid condensation. All the experiments were repeated at least three times to check the reproducibility. The deviation of experimentally obtained results was less than  $\pm 1\%$ .

#### 2.2. Characterization of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

The procedures of characterization of Cu-ZnO/ $Al_2O_3$  were performed in the same manner as reported in the previous paper [12]. The atomic ratio of Cu:Zn:Al of the sample was measured by energy-dispersion X-ray spectroscopy (EDX,

KEVEX, Sigma). BET specific surface area was determined by N<sub>2</sub> adsorption at 77 K. XRD (powder X-ray diffraction) patterns were recorded by X-ray diffractometry (RINT 2000, Rigaku) using Cu K $\alpha$ radiation. The surface of sample was examined by X-ray photoelectron spectroscopy (XPS, ESCA-3200, Shimadzu) with an Mg K $\alpha$  X-ray source operating at 8 kV and 20 mA. The Cu 2p, Zn 2P, Al 2p, O 1s and C 1s levels' spectra were investigated and their binding energies were calibrated using the main peak of the C 1s level spectrum of contaminated carbon at 284.8 eV as an internal reference.

# 3. Results and discussion

## 3.1. Characterization of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub>

The atomic proportion of Cu:Zn:Al in the bulk of the obtained sample was 39.7:40.8:19.5, respectively. The specific surface area was  $68.7 \text{ m}^2 \text{ g}^{-1}$ . Several peaks assignable to ZnO and CuO and some other peaks were observed in the XRD pattern of the untreated sample, showing that the sample was a mixture. The surface atomic ratio of Cu/Zn was calculated from the ratio of the peak area of the Cu 2p level and that of the Zn 2p level in XPS [12], using the set of elemental sensitivity factors of the equipment. The ratio of Cu/Zn was 0.88. We reported the change of the catalyst surface

observed by XPS [13]. The spectra of Cu 2p showed the amount of Cu(I) increased at the expense of Cu(II) after the reaction. We assumed that the active site was the reduced copper species on ZnO.

# 3.2. The effects of reaction pressures on $CH_4$ activation and $C_1$ -oxygenates selectivity in the absence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

The increase of reaction pressures lowered the initiation temperature of methane activation in the selective oxidation of methane with O2 and NO (Fig. 1). This enhancement of methane activation under a higher reaction pressure was similar to that reported in the gas-phase selective oxidation of methane with O<sub>2</sub> [2]. The leveling-off of methane conversion around 6% shows that all of the oxygen in a feed gas (CH<sub>4</sub>/O<sub>2</sub> = 13.3) was used up at around these reaction temperatures. The obtained selectivity of total C<sub>1</sub>-oxygenates and the ratio of CH<sub>3</sub>OH/C<sub>1</sub>-oxygenates in the products was shown as functions of reaction pressures (Fig. 2). We measured the selectivity of C1-oxygenates under the conditions where  $O_2$  conversion exceeded 99%. The ratio of CH<sub>4</sub>/O<sub>2</sub> was kept constant at 13.3. All conversions were included in the region of 5.3-5.7%. C<sub>1</sub>-oxygenates selectivity was raised in a lower region than 1.0 MPa, and it had a maximum value

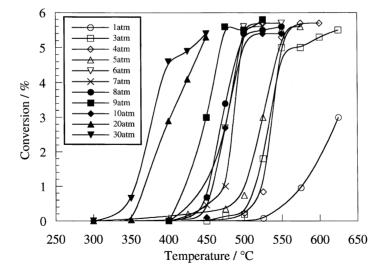


Fig. 1. Effects of reaction pressures on CH<sub>4</sub> conversions in the absence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Feed gas composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, balance; and flow rate:  $120 \text{ ml min}^{-1}$ .

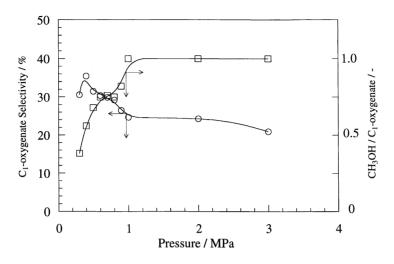


Fig. 2. Effects of reaction pressures on C<sub>1</sub>-oxygenates selectivities and the ratio of CH<sub>3</sub>OH to C<sub>1</sub>-oxygenates in the absence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Feed gas composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, balance; and flow rate: 120 ml min<sup>-1</sup>; gas-phase reaction temperatures: 625 °C (0.3 MPa), 575 °C (0.4 MPa), 550 °C (0.5 MPa), 525 °C (0.6–1.0 MPa), 450 °C (2.0 and 3.0 MPa), respectively. All of the O<sub>2</sub> conversions were higher than 99%. All of the CH<sub>4</sub> conversions were in the range of 5.3–5.7%.

at 0.4 MPa. The decrease of C<sub>1</sub>-oxygenate selectivity at 0.3 MPa could be derived from its higher reaction temperature ( $625 \,^{\circ}$ C), the reaction at 0.4 MPa was conducted at 575 °C. In contrast, the ratio of CH<sub>3</sub>OH/C<sub>1</sub>-oxygenates decreased in the same region. This means the selectivity of CH<sub>2</sub>O increased in this region. The increase of CH<sub>2</sub>O selectivity in a lower pressure region was also reported by Arutyunov et al. in the selective oxidation of methane with O<sub>2</sub> [2].

# 3.3. The effects of reaction pressures on the selectivities of products in the presence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

All of the product selectivities at our reaction pressures are examined in the presence and absence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst were listed in Table 1. The catalyst temperature was kept constant at 250 °C because the selectivity of produced CH<sub>3</sub>OH had a maximum

Table 1

The effects of reaction pressures on the selectivities of products in the presence and absence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub><sup>a</sup>

Number	Pressure (MPa)	Temperature (°C)	Catalasis (g)	Conversion (%)		Selectivity (%)						
				CH <sub>4</sub>	O <sub>2</sub>	CH <sub>3</sub> OH	CH <sub>2</sub> O	CO	CO <sub>2</sub>	$C_2H_4$	$C_2H_6$	CH <sub>3</sub> NO <sub>2</sub>
1	0.4	575	0 <sup>b</sup>	5.5	99	20	15.5	58.9	4.8	0	0.5	0.3
2	0.4	575	0.5	5.5	99.7	32.1	0	51.8	15.2	0	0.5	0.4
3	0.5	550	$0^{b}$	5.5	99	21.4	10.1	63.3	4.4	0	0.8	0
4	0.5	550	0.5	5.4	99.5	28.8	0.1	60.2	9.5	0	1	0.4
5	0.6	525	$0^{b}$	5.6	99	22.9	7.5	59.9	5.6	0.5	0.5	3.2
6	0.6	525	0.5	5.5	99.7	26.1	0	58.7	14	0	0.8	0.4
7	1	525	$0^{b}$	5.4	99.5	24.7	0	65.5	5.2	0	4.2	0.4
8	1	525	0.5	5.6	99.7	24.7	1.8	59.7	8	0.3	4.3	1.2
9	2	450	$0^{b}$	5.3	99.7	24.3	0	59.9	8	0.1	3.7	4
10	2	450	0.5	5.4	99.6	25.4	0	56	13.7	0.9	2	2
11	3	450	$0^{b}$	5.4	99.4	20.9	0	60.4	12.6	0.6	3.4	2.1
12	3	450	0.5	5.5	99.7	24.5	0	55.9	15.1	0.4	1.2	2.9

<sup>a</sup> Catalyst, Cu:Zn:Al = 39.7:40.8:19.5, flow rate: 120 sccm, reaction time: 180 min, catalysts bed temperature: 250 °C and feed gases composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar,16.2%.

<sup>b</sup> In the absence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst.

value at around 250 °C in our previous work [12]. The conversions of CH<sub>4</sub> were around 5.5% irrespective of whether the catalyst was present or not. All the oxygen in the feed gas was used up in the presence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. The selectivities of CH<sub>3</sub>OH and CO<sub>2</sub> in the products were raised in the presence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst, while those of CH<sub>2</sub>O and CO decreased in the presence of the catalyst.

Concerning the increase of  $CH_3OH$  selectivity, we confirmed the presence of hydrogenation reaction between the produced  $CH_2O$  and  $H_2$ 

$$CH_2O + H_2 = CH_3OH \tag{1}$$

on the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst from both experimental results and theoretical calculations of thermodynamic equilibrium values [12]. Concerning the production of H<sub>2</sub> in Eq. (1), we suggested the coexistence of the WGSR between CO and H<sub>2</sub>O on the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst from the experiments between CO and H<sub>2</sub>O.

$$CO + H_2O = CO_2 + H_2 \tag{2}$$

Furthermore, we also suggested the dissociation reaction of CH<sub>2</sub>O on the catalyst as follows:

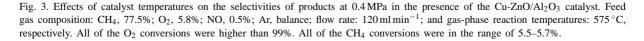
$$CH_2O = CO + H_2 \tag{3}$$

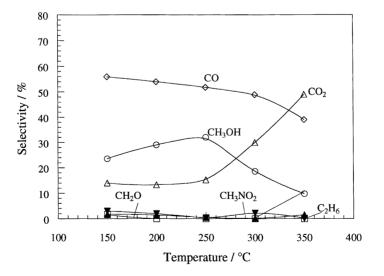
# 3.4. The effects of catalyst temperatures on the selectivities of products

Fig. 3 shows the effects of catalyst temperatures on the selectivities of products at 0.4 MPa in the presence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst because the selectivity of CH<sub>3</sub>OH had a maximum value at 0.4 MPa in Table 1. The reaction conditions other than pressure and temperature were the same as those in Table 1. The conversions of O<sub>2</sub> exceeded 99% at any temperature. CH<sub>2</sub>O was hardly observed in all of the examined regions. CH<sub>3</sub>OH selectivity increased up to 250 °C, then decreased. CO selectivity slightly decreased with increase of catalyst temperatures, and decreased remarkably over 300 °C. CO<sub>2</sub> selectivity rapidly increased over 250 °C. Breen et al. [15] reported that the reactivity of the steam reforming of methanol over the Cu-ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst was raised over around 350 °C. We assumed that the steam reforming reaction between the produced CH<sub>3</sub>OH and H<sub>2</sub>O on Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> progressed over 250 °C at 0.4 MPa.

$$CH_3OH + H_2O = CO_2 + 3H_2$$
 (4)

Figs. 4–6 show the effects of catalyst temperatures on the selectivities of  $CH_3OH$ , CO and  $CO_2$ , respectively. The reaction conditions other than





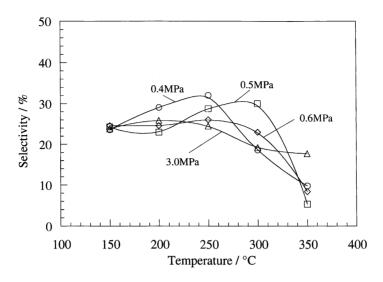


Fig. 4. Effects of catalyst temperatures on CH<sub>3</sub>OH selectivity at 0.4 MPa in the presence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Feed gas composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, balance; flow rate:  $120 \text{ ml min}^{-1}$ ; and gas-phase reaction temperatures:  $575 \degree C$  (0.4 MPa),  $550 \degree C$  (0.5 MPa),  $525 \degree C$  (0.6 MPa),  $450 \degree C$  (3.0 MPa), respectively. All of the O<sub>2</sub> conversions were higher than 99%. All of the CH<sub>4</sub> conversions were in the range of 5.3–5.7%.

pressure were the same as those in Fig. 3.  $CH_3OH$  selectivity increased up to 250 °C at 0.4 MPa (Fig. 4). This increase of  $CH_3OH$  selectivity in a lower temperature region was suppressed under a higher pressure. The decrease of  $CH_3OH$  selectivity in the

region over 250 °C was clearly observed but this decrease was mitigated under a higher pressure. These results show that not only the hydrogenation reaction of CH<sub>2</sub>O, but also the steam reforming reaction was retarded in a higher pressure region. The maximum

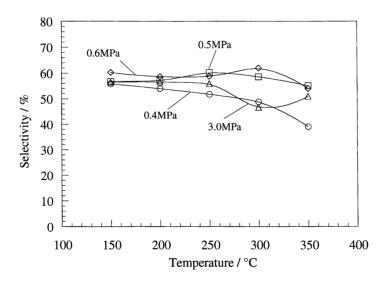


Fig. 5. Effects of catalyst temperatures on CO selectivity at 0.4 MPa in the presence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Feed gas composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, balance; flow rate: 120 ml min<sup>-1</sup>; and gas-phase reaction temperatures: 575 °C (0.4 MPa), 550 °C (0.5 MPa), 525 °C (0.6 MPa), 450 °C (3.0 MPa), respectively. All of the O<sub>2</sub> conversions were higher than 99%. All of the CH<sub>4</sub> conversions were in the range of 5.3–5.7%.

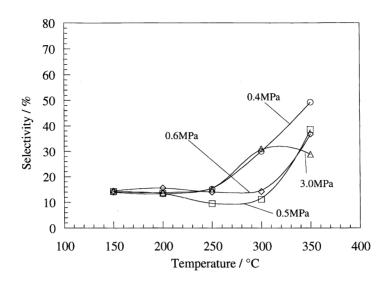


Fig. 6. Effects of catalyst temperatures on CO<sub>2</sub> selectivity at 0.4 MPa in the presence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Feed gas composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, balance; flow rate: 120 ml min<sup>-1</sup>; and gas-phase reaction temperatures: 575 °C (0.4 MPa), 550 °C (0.5 MPa), 525 °C (0.6 MPa), 450 °C (3.0 MPa), respectively. All of the O<sub>2</sub> conversions were higher than 99%. All of the CH<sub>4</sub> conversions were in the range of 5.3–5.7%.

value of CH<sub>3</sub>OH selectivity (32.1%) was obtained at 0.4 MPa and at 250  $^{\circ}$ C.

The variations of CO selectivities were not clear in all the examined reaction temperatures and pressures (Fig. 5). This means that the effects of catalyst temperatures and pressures on the CO related reactions, i.e. Eqs. (2) and (3) were small in the examined region.

As mentioned above, the steam reforming reaction was favorable over  $350 \,^{\circ}$ C. The variation of CO<sub>2</sub> selectivities increased in that region (Fig. 6). However,

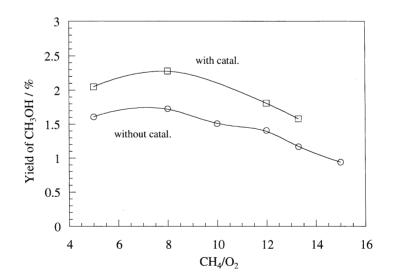


Fig. 7. Effects of CH<sub>4</sub>/O<sub>2</sub> ratios on CH<sub>3</sub>OH yield at 0.4 MPa in the presence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Feed gas composition: CH<sub>4</sub>, 77.5%; O<sub>2</sub>, 5.8%; NO, 0.5%; Ar, balance; flow rate: 120 ml min<sup>-1</sup>; and gas-phase reaction temperatures: 575 °C (0.4 MPa), respectively. All of the O<sub>2</sub> conversions were higher than 99%. All of the CH<sub>4</sub> conversions were in the range of 5.3–5.7%.

this increase was suppressed under a higher pressure as suggested in Fig. 4.

# 3.5. The effects of $CH_4/O_2$ ratios on the selectivities of products

Finally, we examined the effects of CH<sub>4</sub>/O<sub>2</sub> ratio on CH<sub>3</sub>OH yield at 0.4 MPa in the presence and absence of the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. The variations of CH<sub>3</sub>OH yields as functions of CH<sub>4</sub>/O<sub>2</sub> ratio in the presence and absence of the catalyst were almost the same. In the presence of the catalyst, CH<sub>3</sub>OH yields were larger than in the absence of Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> (Fig. 7) in the examined region. CH<sub>3</sub>OH yield had a maximum value at CH<sub>4</sub>/O<sub>2</sub> = 8.0 in the presence of the catalyst.

## 4. Conclusions

The yield of CH<sub>3</sub>OH from CH<sub>4</sub>–O<sub>2</sub>–NO<sub>x</sub> was enhanced by using the Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst in all the examined reaction pressures from 0.4 up to 3.0 MPa. The optimum reaction conditions of the catalyst for the highest yield of CH<sub>3</sub>OH were 250 °C at 0.4 MPa. The highest yield of CH<sub>3</sub>OH was 2.3% at 0.4 MPa and CH<sub>4</sub>/O<sub>2</sub> = 8.0.

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